

PHYSICS 204 A

Fall , 2010

HW #1 SOLUTIONS

Problem 1 :

GOLDBART-STONE 1.3

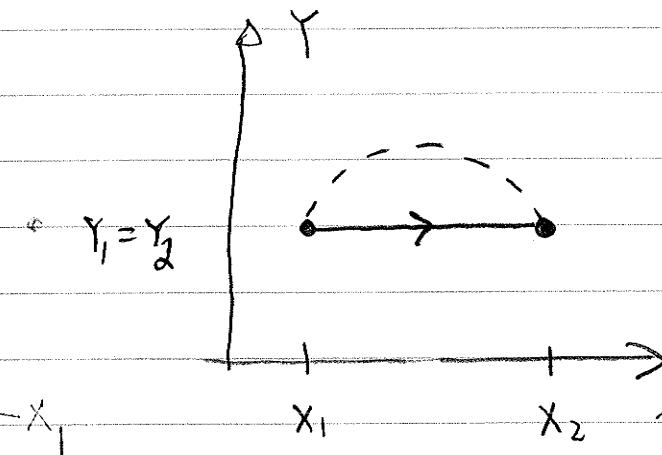
1-1

Hyperbolic Geometry

(The non Euclidean geometry of Lobachevsky)

Metric $ds^2 = \frac{dx^2 + dy^2}{y^2}$ ($y > 0$)

physically this means "distance traveled" is less
as one moves to higher y values.



Instead of —

should go to higher y
to minimize "distance" — —

$$\int_{x_1}^{x_2} \frac{(1+y'^2)^{1/2}}{y} dx$$

$$\frac{\partial f}{\partial y} - \frac{\partial}{\partial x} \left(\frac{\partial f}{\partial y'} \right) = -\frac{(1+y'^2)^{1/2}}{y^2} - \frac{\partial}{\partial x} \left(\frac{(1+y'^2)^{-1/2}}{2} \frac{1}{y} \partial y' \right)$$

Could work through algebra, but we know general principle
since f is indep of $x \rightarrow f - y^1 \frac{\partial f}{\partial y^1} = c$

$$\frac{(1+y'^2)^{1/2}}{y} - y^1 \frac{(1+y'^2)^{-1/2}}{y} y^1 = \frac{1}{R} \quad \text{call constant } \frac{1}{R}$$

Multiply by $\gamma \sqrt{1+\gamma^2}$ yields

$$1 + \gamma^2 - \gamma^2 = \frac{1}{R} \gamma \sqrt{1+\gamma^2}$$

Thus $\frac{R}{\gamma} = \sqrt{1+\gamma^2}$ $\frac{R^2}{\gamma^2} - 1 = \gamma^2$ $\sqrt{\frac{R^2 - \gamma^2}{\gamma^2}} = \frac{dy}{dx}$

Finally $\frac{\gamma dy}{\sqrt{R^2 - \gamma^2}} = dx$ or $-(R^2 - \gamma^2)^{1/2} = x + a$

so $R^2 - \gamma^2 = (x+a)^2$ $(x+a)^2 + y^2 = R^2$

circle center at $(-a, 0)$ radius R ,

Given points (x_1, y_1) (x_2, y_2) how are a, R determined

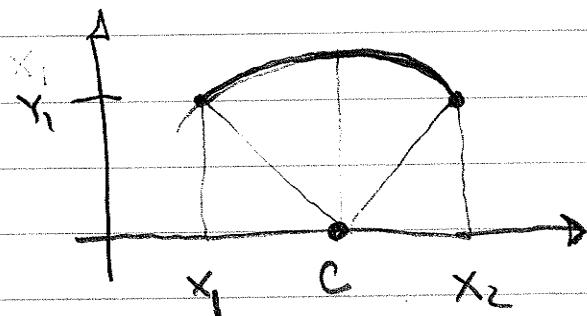
$$\begin{aligned} (x_1 + a)^2 + y_1^2 &= R^2 \\ (x_2 + a)^2 + y_2^2 &= R^2 \end{aligned} \Rightarrow (x_1 + a)^2 + y_1^2 = (x_2 + a)^2 + y_2^2$$

+ get a

$$\begin{aligned} x_1^2 + 2ax_1 + a^2 + y_1^2 &= \\ x_2^2 + 2ax_2 + a^2 + y_2^2 &= \end{aligned}$$

$$a = \frac{x_1^2 - x_2^2 + y_1^2 - y_2^2}{2(x_2 - x_1)}$$

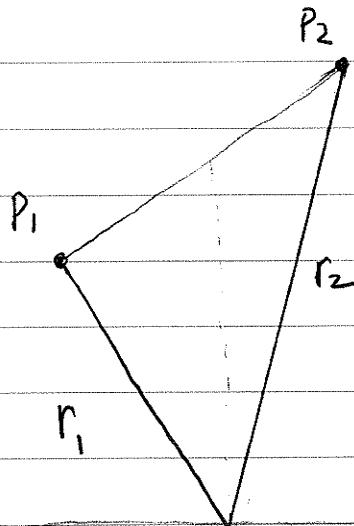
Special case $y_1 = y_2$ $-a = \left(\frac{x_1 + x_2}{2}\right)$ as expected



$$R^2 = y_1^2 + \left(\frac{x_1 - x_2}{2}\right)^2$$

(Pythagorean thm)

Geometrical construction:

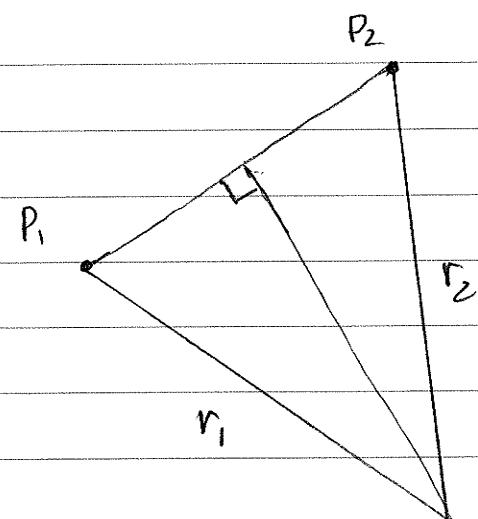


$$\text{Using } -a = \frac{x_1 + x_2}{z}$$

evidently will fail since
 $r_1 \neq r_2$

Must move to right.

pretty clearly $r_1 = r_2$ when using \perp bisector



by "SAS"

Page C113B shows

mathematically that $(-a, 0)$

is indeed on \perp bisector.

Recast Egn in clever way

$$\frac{y_2^2 - y_1^2}{2} = \frac{x_1^2 - x_2^2}{2} + a(x_1 - x_2)$$

$$\left(\frac{y_1 + y_2}{2}\right)\left(y_2 - y_1\right) = (x_1 - x_2) \left[\frac{x_1 + x_2}{2} + a \right]$$

$$\frac{-y_1 + y_2}{2} = \frac{x_1 - x_2}{y_2 - y_1} \left[-a - \frac{x_1 + x_2}{2} \right]$$

Think about this as egn of line

$$y - y_0 = m(x - x_0)$$

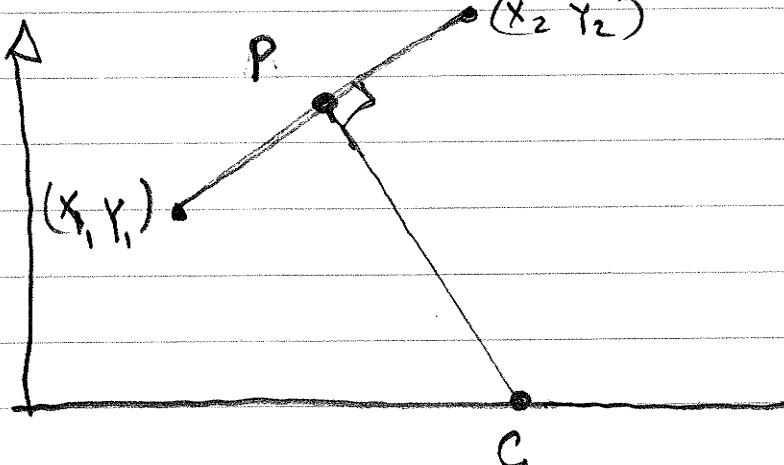
through point $(-a, 0) = (x_0, y_0)$

Evidently $y_0 = \frac{y_1 + y_2}{2}$ $x_0 = \frac{x_1 + x_2}{2}$

what is this point? Midpoint P of (x_1, x_2) (y_1, y_2) !

slope of line is $\frac{x_1 - x_2}{y_2 - y_1}$ Does any one recognize this?

It is $-1/m$
where m is slope
of line through P_1, P_2

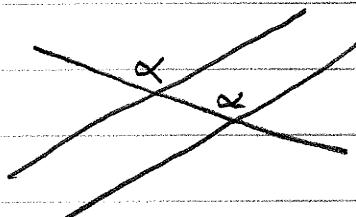


→ perpendicular

Before doing parts b) c) some preliminary comments:

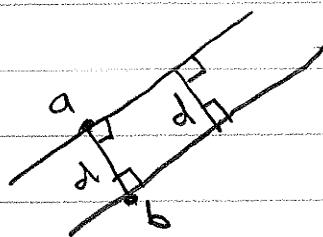
1) In Euclidean geometry there are many equivalent definitions of the word "parallel".

a) 2 lines are parallel if a third line intersects them at the same angle



b) two lines are parallel if they never meet

c) two lines are parallel if the distance between them is constant.



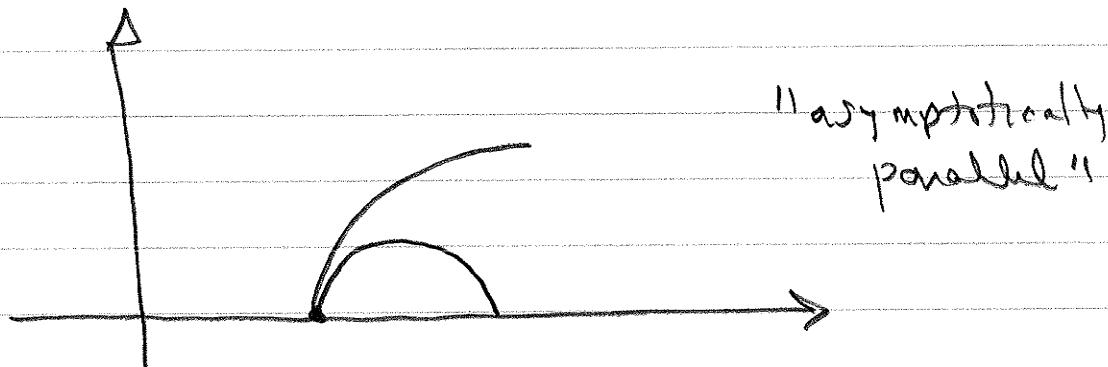
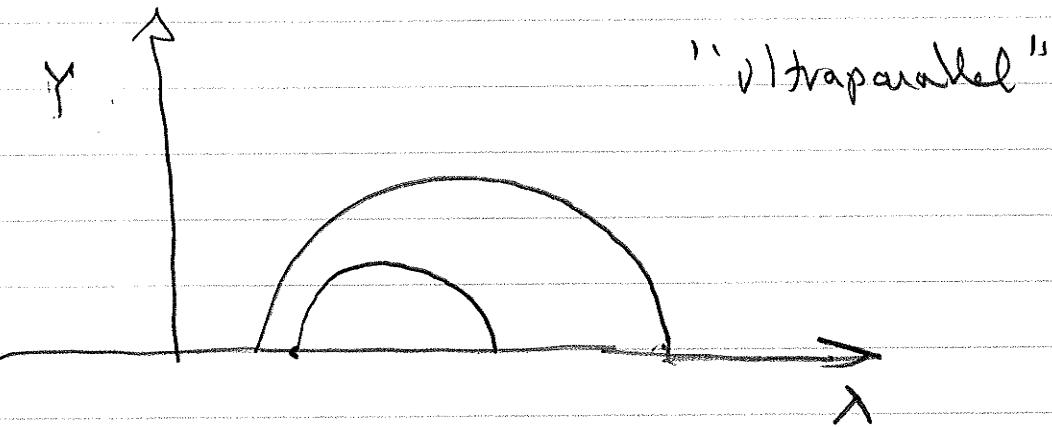
← (This picture raises question about how points a/b chosen)

In non Euclidean geometries these definitions are inequivalent?

2) So the textbook adopts the definition that lines are parallel if they meet at infinity at one end, that is definition to do the problem as stated. The definition sort of makes sense in that at one end at least it is a version of c. Clearly 2 lines in this geometry must touch on the x-axis or else the distance between them is infinite. (It only sort of works because of presence of non touching end)

3) This is apparently not the usual nomenclature.

Carly says word "parallel" is not usually used
in this geometry.



b) Uniqueness follows from algebra/geometric construction:

There is only one way to do it!

$$c) (x+a)^2 + y^2 = R^2$$

$$y = [R^2 - (x+a)^2]^{1/2}$$

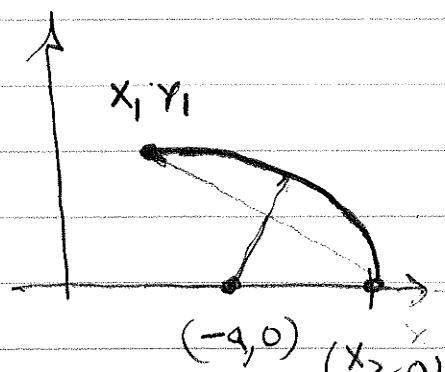
$$\frac{dy}{dx} = [R^2 - (x+a)^2]^{-1/2} [- (x+a)]$$

$$(\frac{dy}{dx})^2 = \frac{(x+a)^2}{R^2 - (x+a)^2}$$

$$1 + (\frac{dy}{dx})^2 = \frac{R^2}{R^2 - (x+a)^2}$$

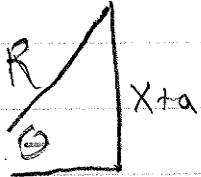
$$\therefore \int_{x_1}^{x_2} \frac{dx}{\sqrt{1 + (\frac{dy}{dx})^2}} = \int_{x_1}^{x_2} \frac{dx}{\sqrt{\frac{R^2}{R^2 - (x+a)^2}}}$$

$$= \int_{x_1}^{x_2} dx \frac{R}{\sqrt{R^2 - (x+a)^2}}$$



$$\text{Note that } y_2 = 0 \Rightarrow (x+a)^2 = R^2$$

$$(x+a) = R \sin \theta \quad dx = R \cos \theta d\theta$$



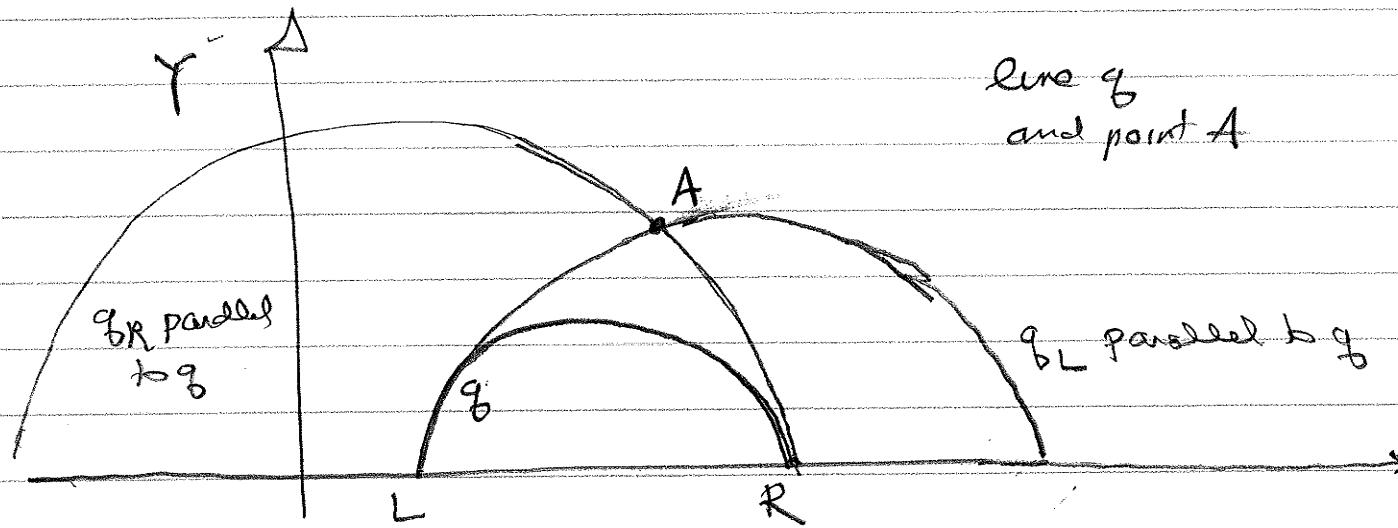
$$\int \frac{R \cos \theta d\theta}{R^2 \cos^2 \theta} \quad R = \int \sec \theta d\theta = \ln(\sec \theta + \tan \theta)$$

Travel time from $(x, y_1) \rightarrow (x_2, 0)$ is

$$\ln(\sec\theta + \tan\theta) = \ln \left[\frac{R + (x+a)}{\sqrt{R^2 - (x+a)^2}} \right]^{x_2}_{x_1}$$

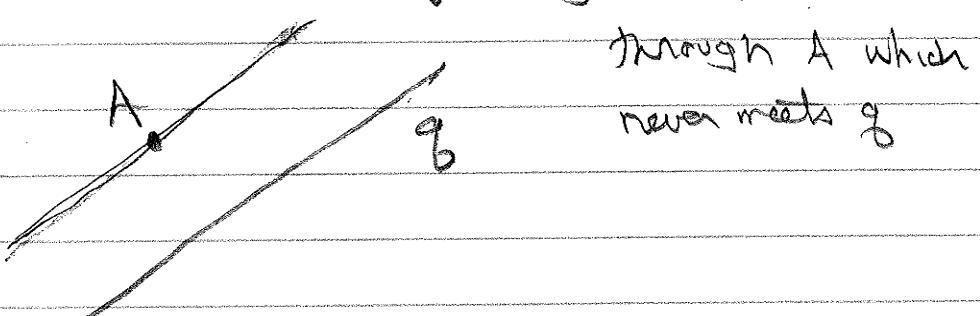
But $R^2 - (x_2+a)^2 = 0 \Rightarrow$ two always \exists

Lines go from $+\infty$ to $-\infty$: Start and end on x-axis



two ways to meet at infinity : left
or Right sides \Rightarrow 2 lines.

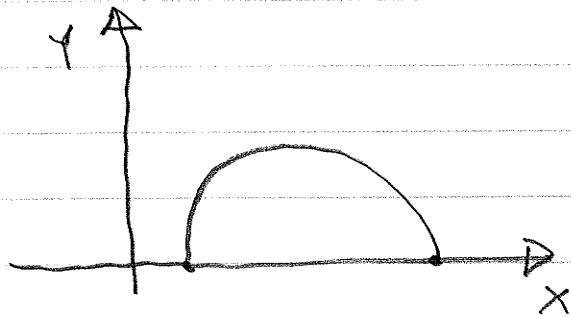
What's point : In "ordinary" geometry only 1 line



Q: What is a line??

A: Can travel along it forever without reaching end.

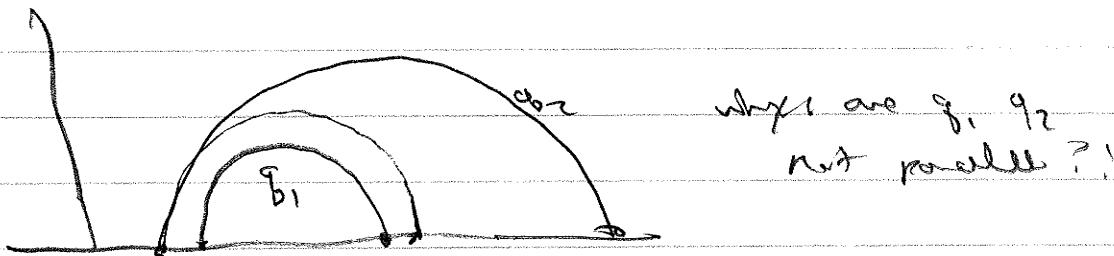
If so, in this geometry, lines begin and end on x-axis



"Usual" geometry: only one line through 2 given points. Same is true here.

"Usual" geometry:

Basic Q: why is nothing at "o" part of definition of parallel. Why not just that they do not meet?!



Physics 204A Fall 2010

Problem Set #1

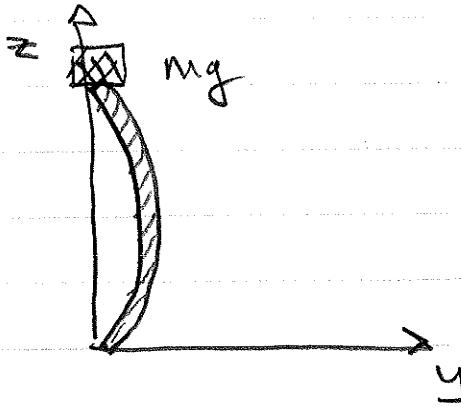
Problem 2 17. Problem Soln of 1.4

Goldbart - Stone 1.4

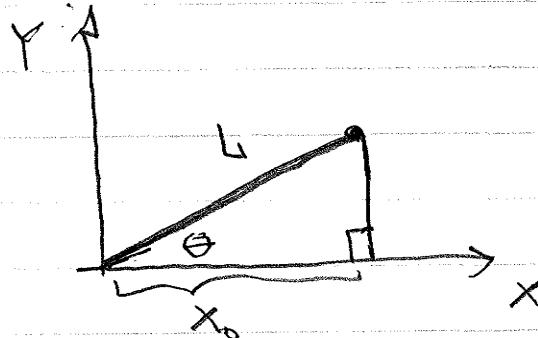
- a) We will first just use the formula for the elastic energy (later we will see where it comes from !!) of the bar

$$U_e = \int_0^L \frac{1}{2} EI y'' dz$$

We need the potential energy of the load mg



How much lower does my fall due to bending?



segment length L

When a line makes an angle θ with an axis

its projection $x_0 = L \cos \theta = L(1 - \theta^2/2)$ if θ is small

Now $\theta \approx \tan \theta = dy/dx$ so $L - x_0 = -\frac{1}{2} (\frac{dy}{dx})^2 L$

Considering a bent shape as a collection of

such segments we see that the load may fully

a distance $\frac{1}{2} \int dz \left(\frac{dy}{dz} \right)^2$

Putting together

$$U[y] = \int_0^L \left[\frac{YI}{2} (y'')^2 - \frac{Mg}{2} (y')^2 \right] dz$$

If $y(z) = \sum_{n=1}^{\infty} a_n \sin \frac{n\pi z}{L}$ ← note $y(0) = y(L) = 0$

$$y'(z) = \sum_{n=1}^{\infty} a_n \frac{n\pi}{L} \cos \frac{n\pi z}{L}$$

$$y''(z) = -\sum_{n=1}^{\infty} a_n \left(\frac{n\pi}{L} \right)^2 \sin \frac{n\pi z}{L}$$

$$\int_0^L \cos \left(\frac{n\pi z}{L} \right) dz = Y_L = \int_0^L \sin \left(\frac{n\pi z}{L} \right) dz$$

$$U(y) = \sum_{n=1}^{\infty} \left[\frac{YI}{2} \left(\frac{n\pi}{L} \right)^4 - \frac{Mg}{2} \left(\frac{n\pi}{L} \right)^2 \right] a_n^2 \frac{L}{2}$$

Unstable if $\frac{YI}{2} \left(\frac{n\pi}{L} \right)^2 < \frac{Mg}{2}$

$$Mg > YI \left(\frac{n\pi}{L} \right)^2$$

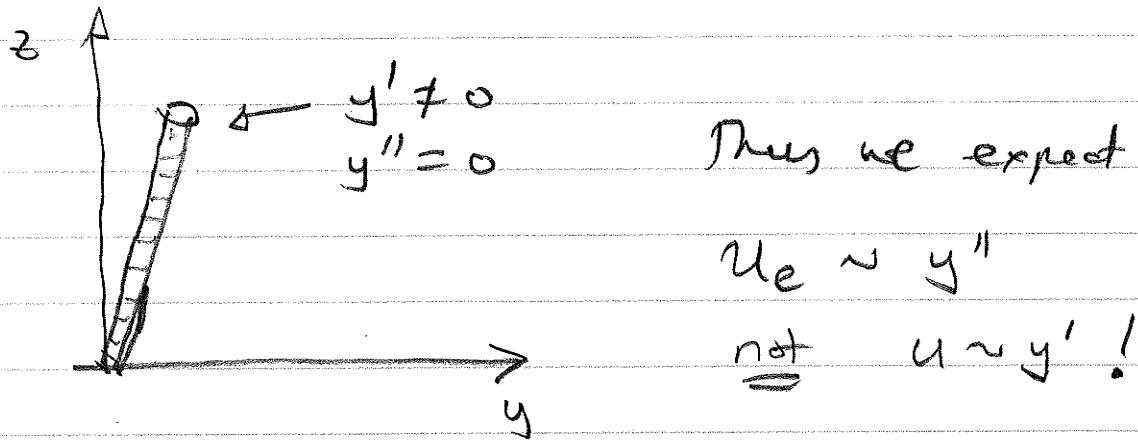
physically reasonable M in numerator
and L in denominator ??

Now where does we come from?

2-3

First comment on $U_e = \int_0^L \frac{1}{2} EI y'' dz$:

clearly if you do not bend the bar but just give it a nonzero y' it remains straight and the elastic energy is zero



Put better: The curvature of a function is not set by the derivative.

constant radius $x^2 + y^2 = R^2$ $y = (R^2 - x^2)^{1/2}$

Then $\frac{dy}{dx} = -x(R^2 - x^2)^{-1/2}$

$\frac{d^2y}{dx^2} = -(R^2 - x^2)^{-1/2} - x^2(R^2 - x^2)^{-3/2}$

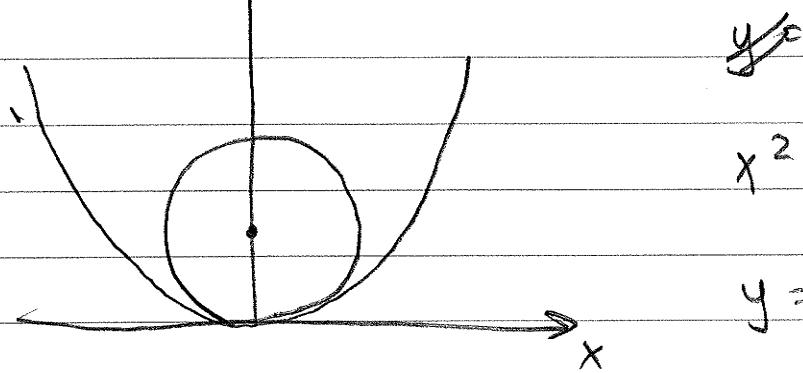
What circle best approximates

$$f(x) = f(x_0) + f'(x_0)(x - x_0) + \frac{1}{2}f''(x_0)(x - x_0)^2 + \dots$$

$$x_0 = 0$$

wlog consider $f(x) = 0 = f'(x_0)$ i.e. orient axes and locate axes at minimum of $f(x)$

$$f(x) = \frac{1}{2}f''(x_0)x^2$$



$$x^2 + (y - R)^2 = R^2$$

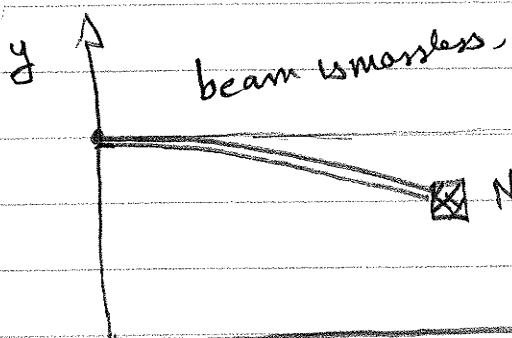
$$y = R - \sqrt{R^2 - x^2}$$

$$= R - R\left(1 - \frac{x^2}{R^2}\right)^{1/2}$$

$$\text{Taylor expand } y = R - R\left(1 - \frac{x^2}{2R^2}\right) = \frac{1}{2}\frac{1}{R}x^2$$

$$\text{Matching up we see } f''(0) \approx 1/R$$

$$(b) \text{ We use } U_e = \int_0^L \frac{\gamma I}{2} (y'')^2 dx$$



$$U = \int_0^L \frac{\gamma I}{2} (y'')^2 + Mg y(L)$$

Question: Why not use

$$\int_0^L y' dx \text{ as distance}$$

(Use x as horiz. axis
not z as stated in text)

Mg falls?

Answer: This is same as
 $y(L)!!$

So, our total energy functional is:

$$U[y] = \int_0^L \frac{\gamma I}{2} (y'')^2 dx + Mg y(L)$$

Applying, integration by parts twice we get!

$$\delta U = \int_0^L \gamma I y'' \delta y'' dx + Mg \delta y(L)$$

$$= \gamma I y'' \delta y' |_0^L - \int_0^L \gamma I \delta y' y''' dx + Mg \delta y(L)$$

$$\delta U = \gamma I y'' \delta y' |_0^L - \gamma I y''' \delta y |_0^L + \int_0^L \gamma I y^4 \delta y dx + Mg \delta y(L)$$

Note: we could not naively apply E-L equations since
endpoints are not fixed, but we are given
specific boundary conditions which help us
solve the problem.

We are given boundary conditions :

At $x=0$, $y(0)=0$ and $y'(0)=0$

which means $y'''(0) = y''(0) = 0$ also

Re-writing SCL (and eliminating zero terms based on above)

$$SCL = V I y''(L) \delta y' - V I y'''(L) \delta y(L) + M g \delta y(L)$$

$$+ \int_0^L V I y^{(4)} \delta y \, dx$$

$$= [V I y''(L)] \delta y' - [V I y'''(L) - M g] \delta y(L) \\ + \left[\int_0^L V I y^{(4)} \, dx \right] \delta y$$

All terms in boxes must vanish at a minimum.

So, we obtain :

$$y''(L) = 0$$

$$y'''(L) = MG/VI$$

From here, we let :

$$y(x) = ax^3 + bx^2 + cx + d \quad [y^{(4)}=0 \text{ above!}]$$

and solve for coefficients :

$$c, d = 0 \text{ since } y(0)=d \text{ and } y'(0)=c$$

$$\text{So } y(x) = ax^3 + bx^2$$

2-7

$$y''(x) = 6ax + 2b \Rightarrow y''(L) = 6aL + 2b = 0$$

$b = -3aL$

$$y'''(x) = 6a = Mg/VI \quad a = Mg/6VI$$

Finally)

a b

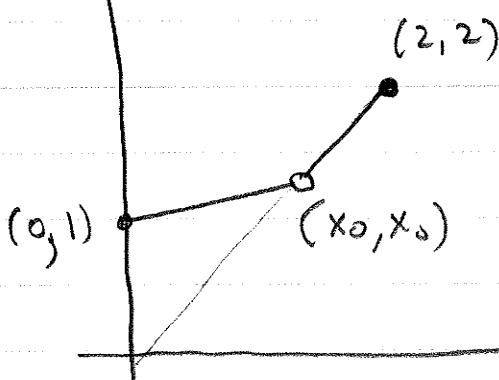
$$y(x) = \frac{Mg}{6VI} x^3 - \frac{3Mg}{6VI} x^2 = \frac{Mg}{6VI} (x^3 - 3Lx^2)$$

and $y(L) = -\frac{1}{3} Mg L^3 / VI$

3-1

Problem 3: Minimize time travel of ray of light

y



(2, 2)

(0, 1)

(x₀, y₀)

$$n = a + b(y^2 - x^2)$$

$$v = c/n$$

$$dt = ds/v = ds n/c$$

$$y = mx + 1$$

$$ds = \sqrt{dx^2 + dy^2} = dx \sqrt{1+m^2} \quad \text{where } m = \frac{x_0 - 1}{x_0}$$

$$t_1(x_0) = \int_0^{x_0} dx \sqrt{1+m^2} \cdot \frac{a+b[(mx+1)^2 - x^2]}{c}$$

$$t_2(x_0) = (2-x_0)\sqrt{2} \frac{a}{c}$$

$$t_1(x_0) = \frac{\sqrt{1+m^2}}{c} \int_0^{x_0} dx \left[a + b[(m^2-1)x^2 + 2mx + 1] \right]$$

$$= \frac{\sqrt{1+m^2}}{c} \left[ax + b(m^2-1)x^3 + mbx^2 + bx \right] \Big|_0^{x_0}$$

$$= \frac{\sqrt{1+m^2}}{c} \left[(a+b)x_0 + mbx_0^2 + b\frac{(m^2-1)}{3}x_0^3 \right]$$

$$\frac{dt}{dx_0} = \frac{d}{dx_0}(t_1 + t_2) \quad \leftarrow \text{Note } n \text{ is a function of } x_0 \text{ here}$$

Program to compute minimum time

3-2

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1

```
c      CODE TO COMPUTE MIN TIME TO TRAVEL FROM (1,0) to (2,2)
c      ALONG GENERAL PATH
c      FOR v=c/n WITH c=1 and n=a+b |y^2-x^2|
c
c      implicit none
real*8 a,b,c,x(0:100),y(0:100),dx,dx2,n,beta,E,dE,move
real*8 dy,ran2,xx,yy,avey(0:100),aveE,aveE2
integer ix,Nx,imonte,Nmonte,iran,accept
c
c      c=1.d0
c      Nx=400
c
c      write (6,*) 'enter a,b,Nmonte,move,beta,iran'
c      read  (5,*)      a,b,Nmonte,move,beta,iran
c
c      dx=2.d0/dfloat(Nx)
c      dx2=dx*dx
c
c      INITIALIZE x,y TO BE STRAIGHT LINE
c
do 100 ix=0,Nx
      x(ix)=0.d0+(2.d0-0.d0)*dfloat(ix)/dfloat(Nx)
      y(ix)=1.d0+(2.d0-1.d0)*dfloat(ix)/dfloat(Nx)
100 continue
c
c      COMPUTE "ENERGY"
c
E=0.d0
do 110 ix=1,Nx
      xx=x(ix)-dx2
      yy=(y(ix)+y(ix-1))/2.d0
      n=a+b*dabs(yy*yy - xx*xx)
      dE = dsqrt( (y(ix)-y(ix-1))**2 + dx2 ) * n/c
      E=E+dE
      avey(ix)=0.d0
110 continue
avey( 0)=1.d0*dfloat(Nmonte)
avey(Nx)=2.d0*dfloat(Nmonte)
c
accept=0
aveE =0.d0
aveE2=0.d0
do 300 imonte=1,Nmonte
do 200 ix=1,Nx-1
c
      xx=x(ix)-dx2
c
      yy=(y(ix)+y(ix-1))/2.d0
      n=a+b*dabs(yy*yy - xx*xx)
      dE = - dsqrt( (y(ix)-y(ix-1))**2 + dx2 ) * n/c
c
      yy=(y(ix)+y(ix+1))/2.d0
      n=a+b*dabs(yy*yy - xx*xx)
      dE = dE - dsqrt( (y(ix)-y(ix+1))**2 + dx2 ) * n/c
c
      dy=move*(ran2(irand)-0.5d0)
c
      yy=(y(ix)+dy+y(ix-1))/2.d0
      n=a+b*dabs(yy*yy - xx*xx)
      dE = dE + dsqrt( (y(ix)+dy-y(ix-1))**2 + dx2 ) * n/c
c
      yy=(y(ix)+dy+y(ix+1))/2.d0
      n=a+b*dabs(yy*yy - xx*xx)
      dE = dE + dsqrt( (y(ix)+dy-y(ix+1))**2 + dx2 ) * n/c
```

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2

```

        if (ran2(irand).le.dexp(-beta*dE)) then
            accept=accept+1
            y(ix)=y(ix)+dy
            E=E+dE
        endif
        avey(ix)=avey(ix)+y(ix)
        aveE =aveE +E
c         aveE2=aveE2+E*E
200     continue
300     continue
        aveE =aveE /(dfloat(Nx-1)*dfloat(Nmonte))
c         aveE2=aveE2/(dfloat(Nx-1)*dfloat(Nmonte))

c         NEED TO BIN TO GET ACCURATE ERROR ESTIMATE...

        write (6,990) dfloat(accept)/(dfloat(Nx-1)*dfloat(Nmonte)),
c         1     aveE,dsqrt(aveE2-aveE*aveE)/dsqrt(dfloat(Nmonte-1))
1     E,aveE
c990    format('acc= ',f8.4,' <t>= ',f8.4,' +- ',f8.4)
990    format('acc= ',f8.4,' <t>= ',f8.4,'      t= ',f8.4)
991    format(i6,3f8.4)

        do 400 ix=0,Nx
            write (66,991) ix,x(ix),y(ix),avey(ix)/dfloat(Nmonte)
400     continue

        end

c         USE THESE COMMENTED OUT LINES IF REAL*8 DESIRED.
REAL*8 FUNCTION RAN2(IDUM)
IMPLICIT REAL*8(A-H,O-Z)
c         FUNCTION RAN2(IDUM)
save
PARAMETER (M=714025,IA=1366,IC=150889,RM=1.4005112E-6)
DIMENSION IR(97)
DATA IFF /0/
IF(IDUM.LT.0.OR.IFF.EQ.0)THEN
    IFF=1
    IDUM=MOD(IC-IDUM,M)
    DO 11 J=1,97
        IDUM=MOD(IA*IDUM+IC,M)
        IR(J)=IDUM
11    CONTINUE
    IDUM=MOD(IA*IDUM+IC,M)
    IY=IDUM
ENDIF
J=1+(97*IY)/M
IF(J.GT.97.OR.J.LT.1)PAUSE
IY=IR(J)
RAN2=IY*RM
IDUM=MOD(IA*IDUM+IC,M)
IR(J)=IDUM
RETURN
END

```

